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# The Reynolds transport theorem for three phase systems with interface storage

## Introduction

The Reynolds Transport Theorem (since abbreviated RTT) is a kinematic relation expressing the accumulation rate of an Extensive Quantity ( $EQ$ ) in a material system  $\Sigma$  given by Lagrangian description in terms referenced to a domain of spatially prescribed configuration (*Eulerian* description) of volume  $V$  (fixed or movable). The first RTT for heterogeneous systems of negligible interface storage is by Truesdell and Toupin [1]. If, however, contribution of the interface storage into system storage can be essential Slattery [2] proposed the RTT as

$$\frac{d}{dt} = \left( \int_{\Omega} \eta dV + \int_{\Gamma} \eta_s dA \right) = \int_V \left( \frac{D\eta}{Dt} + \eta \operatorname{div} \mathbf{V} \right) dV + \int_S \left( \frac{D_s \eta_s}{Dt} + \eta_s \operatorname{div}_S \mathbf{V}_s + \|\eta(\mathbf{V} - \mathbf{U}) \cdot \boldsymbol{\zeta}\| \right) dA \quad (1)$$

where  $V$  stands for an established fixed volume of reference (*Eulerian* description),  $S$  is the overall interface area within  $V$ .  $\mathbf{U}$  and  $\mathbf{V}_s$  are the spatial velocities of the interfaces and the surface systems moving in, respectively.  $D\eta/Dt$  and  $D_s \eta_s / Dt$  stand for the material derivatives of spatial and surface densities  $\eta$  and  $\eta_s$ , respectively. Term  $\|\eta(\mathbf{V} - \mathbf{U}) \cdot \boldsymbol{\zeta}\|$  of Eq.(1) reads as  $\|\eta^+(\mathbf{V}^+ - \mathbf{U}) \cdot \boldsymbol{\zeta}^+ + \eta^-(\mathbf{V}^- - \mathbf{U}) \cdot \boldsymbol{\zeta}^-\|$  where  $\boldsymbol{\zeta}$  means the outward unit normal vector to the interface pointing into phase moving at  $V$  and refers to the jump condition for phasic spatial density  $\eta$  across the interface set between two phases which properties are denoted by superscripts  $+$  and  $-$ . Single integral symbols  $\int$  used throughout the paper refer to either the volume (differential  $dV$ ), surface ( $dA$ ) or line ( $dl$ ) integrals, respectively.

This paper is purposed to derive the RTT relation for three phase systems of essential interface storage in terms referenced to control volume  $CV$  surrounded by control surface  $CS$  being in arbitrary motion with respect to fixed (inertial) reference frame.

## RTT for three phase systems

In Fig. 1 a three phase material system  $\Sigma$  is displayed occupying spatial domain  $\Omega$  of boundary  $\Gamma$  split into phasic portions  $\Omega_i$  ( $i = 1, 2, 3$ ). The system is composed of three spatial subsystems  $\bigcup_i^3 \Sigma_{vi}$  separated by interfaces  $S$  and  $K$  surface subsystems  $\bigcup_k^K \Sigma_{sk}$  dwelling in  $S$ . System passes through a movable  $CV$  bounded by  $CS$ , see in Fig. 2a. In view of  $\Sigma$  is composed of spatial and surface subsystems the  $CV$  comprises both spatial phasic domains of total volume  $V$  and interfacial domains of aggregated area  $S$ , hence  $CV = V \cup S$ .

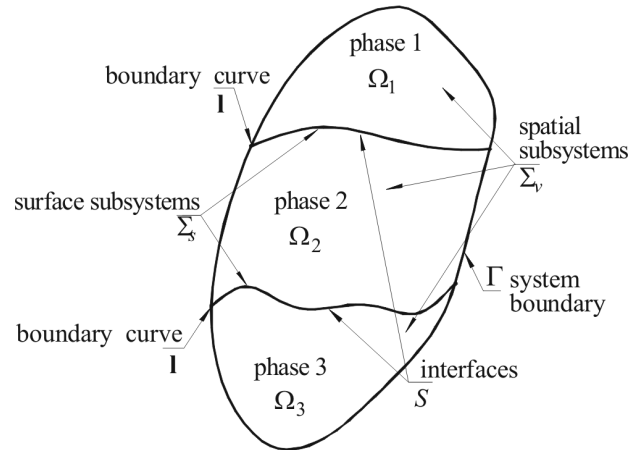


Fig. 1. System  $\Sigma$  composed of spatial and surface subsystems

Volume  $V$  involves all the phasic volumes embedded in  $CV$ , hence  $V = \bigcup_i^3 V_i$ . The aggregated interfacial area  $S$  involves the interfaces placed within  $CV$  so that  $S = \bigcup_k^K S_k$ . The entire  $CS$  consists in  $CS = R \cup C$  where  $R$  is the aggregated external boundary of phasic domains determined as  $R = \bigcup_i^3 R_i$  with understanding that each  $R_i$  is the entire external boundary accompanying the  $i^{th}$  phasic volume.  $C = \bigcup_k^K C_k$  stands for the aggregated boundary curve of all individual boundary curves  $C_k$  formed as intersection of  $CS$  and interface  $S_k$ .

Accumulation  $\delta\Phi_\Sigma$  of an extensive quantity (abbreviated  $EQ$ ) in system  $\Sigma$  is determined by the difference in system storages  $\Phi_\Sigma$  at  $t + \delta t$  and  $t$ , hence

$$\underbrace{\delta\Phi_\Sigma}_{\text{accumulation in } \Sigma \text{ during } \delta t} = \underbrace{\Phi_\Sigma(t + \delta t)}_{\text{storage in } \Sigma \text{ at } t + \delta t} - \underbrace{\Phi_\Sigma(t)}_{\text{storage in } \Sigma \text{ at } t} \quad (2)$$

In Fig. 2a the coincidence of  $\Omega$  and  $CV$  is shown at an instant  $t$ . In such particular circumstances boundary  $\Gamma$  of system  $\Sigma$  traced by lowercase letters  $abcdefa$  is superimposed upon boundary  $CS$  of  $CV$  indicated by  $ghijklg$ , hence  $abcdefa = ghijklg$ , (Fig. 2a). In turn amounts of  $EQ$  stored within  $\Sigma$  and  $CV$  are the same, what gives

$$\underbrace{\Phi_\Sigma(t)}_{\text{storage in } \Sigma \text{ at } t} = \underbrace{\Phi_{CV}(t)}_{\text{storage in } CV \text{ at } t} \quad (3)$$

At instant  $t + \delta t$  system  $\Sigma$  is displaced partially out of  $CV$ . Hence, boundaries of  $\Sigma$  traced along  $abcdefa$  and  $CV$  marked as  $ghijklg$  are shifted each other (Fig. 2b).

In turn, system  $\Sigma$  leaves to  $CV$  some amount of  $EQ$  stored in region  $I$  ( $afedjklga$ ) and carries out of  $CV$  some amount of  $EQ$  stored in region  $II$  ( $abcdihg$ ). Hence, based on Fig. 2b one gets storage  $\Phi_\Sigma(t + \delta t)$  expressed in terms referenced to  $CV$  as

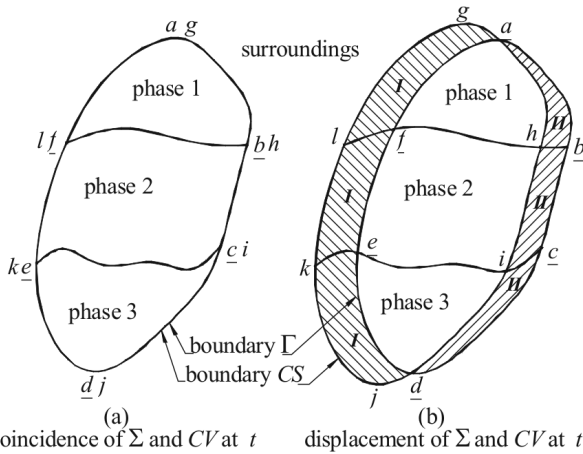


Fig. 2. System  $\Sigma$  passing through a moving CV: a) coinciding condition at time  $t$ ; b) displacement of  $\Sigma$  with respect to CV at time  $t + \delta t$

$$\underbrace{\Phi_{\Sigma}(t + \delta t)}_{\text{storage in } \Sigma \text{ at } t + \delta t} = \underbrace{\Phi_{CV}(t + \delta t)}_{\text{storage in CV at } t + \delta t} + \underbrace{\delta\Phi_{II}(\delta t)}_{\text{amount of EQ carried by } \Sigma \text{ out of CV during } \delta t \text{ (region II)}} - \underbrace{\delta\Phi_I(\delta t)}_{\text{amount of EQ brought in CV by } \Sigma \text{ during } \delta t \text{ (region I)}} \quad (4)$$

where  $\delta\Phi_I(\delta t)$  stands for inflow of EQ into CV across CS. Term  $\delta\Phi_{II}(\delta t)$  of Eq. (5) means the efflux of EQ across CS out of CV. By substitution Eqs (3, 4) into Eq. (2) one obtains

$$\underbrace{\delta\Phi_{\Sigma}}_{\text{accumulation in } \Sigma \text{ during } \delta t} = \underbrace{\Phi_{CV}(t + \delta t) - \Phi_{CV}(t)}_{\text{accumulation in moving CV}} + \underbrace{\delta\Phi_{II}(\delta t) - \delta\Phi_I(\delta t)}_{\text{transport across CS}} \quad (5)$$

Storages  $\Phi_{CV}(t)$  and  $\Phi_{CV}(t + \delta t)$  of Eq.(5) include those in the spatial domains of volume  $V$  (denoted by  $\Phi_V$ ) and those in the interfacial domains of area  $S$  (by  $\Phi_S$ ). Likewise, amounts of EQ transported by moving  $\Sigma$  refer to contributions made by macroscopic movements of both spatial (by  $\delta_s\Phi$ ) and surface (by  $\delta_s\Phi$ ) subsystems. With this understanding, corresponding terms are introduced into Eq. (5) and subsequently all the terms on both sides are divided by  $\delta t$ . Then by letting  $\delta t \rightarrow 0$  one gets Eq. (5) expressed on the rate basis as

$$\lim_{\delta t \rightarrow 0} \frac{\delta\Phi_{\Sigma}}{\delta t} = \lim_{\delta t \rightarrow 0} \left[ \underbrace{\frac{\Phi_V(t + \delta t) - \Phi_V(t)}{\delta t}}_{\substack{\text{accumulation rate in} \\ \text{spatial phasic domains} \\ \text{of volume } V \\ (1)}} + \underbrace{\frac{\delta_s\Phi_{II}(\delta t) - \delta_s\Phi_I(\delta t)}{\delta t}}_{\substack{\text{transport rate of EQ by} \\ \text{movement of spatial} \\ \text{subsystems across CS} \\ (2)}} + \underbrace{\frac{\Phi_S(t + \delta t) - \Phi_S(t)}{\delta t}}_{\substack{\text{accumulation rate in} \\ \text{interfacial domains} \\ \text{of area } S \\ (3)}} + \underbrace{\frac{\delta_s\Phi_{II}(\delta t) - \delta_s\Phi_I(\delta t)}{\delta t}}_{\substack{\text{transport rate of EQ by} \\ \text{movement of surface} \\ \text{subsystems across CS} \\ (4)}} \right] \quad (6)$$

The left side of Eq. (6) converges at the accumulation rate of EQ within  $\Sigma$  to be given by

$$\lim_{\delta t \rightarrow 0} \frac{\delta\Phi_{\Sigma}}{\delta t} = \frac{d\Phi_{\Sigma}}{dt} \quad (7)$$

Below, the right side terms of Eq. (6) are converted into rate forms referenced to moving CV.

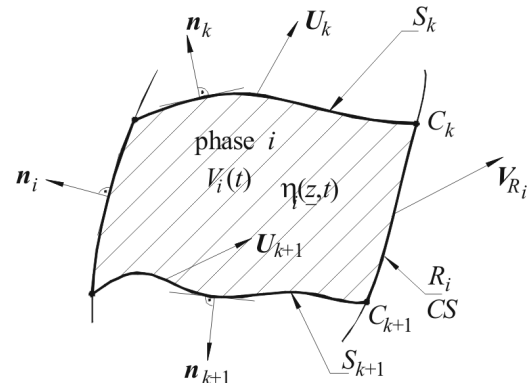


Fig. 3. Phasic domain  $V_i(t)$  bounded by boundary  $R_i$  and moving interfaces  $S_k$  and  $S_{k+1}$

**Term (1)**

Taking the limit the rate form of the first term of Eq. (6) becomes

$$\lim_{\delta t \rightarrow 0} \frac{\Phi_V(t + \delta t) - \Phi_V(t)}{\delta t} = \frac{d\Phi_V(t)}{dt} \quad (8)$$

where:

$$\frac{d\Phi_V(t)}{dt} = \sum_i^3 \frac{d\Phi_{V_i}(t)}{dt} \quad \text{and} \quad \Phi_{V_i}(t) = \int_{V_i(t)} \eta_i(\underline{z}, t) dV \quad (9)$$

is the storage within the  $i^{th}$  phasic domain of moving volume  $V_i(t)$  at an instant  $t$  and  $\underline{z}$  are the spatial coordinates. In Fig. 3 boundaries of volume  $V_i(t)$  are illustrated.

It is seen in Fig. 3 that the entire boundary  $\mathfrak{R}_i$  of  $V_i$  is a closed surface  $\mathfrak{R}_i = R_i + S_i$  where  $R_i$  is the external part of  $\mathfrak{R}_i$  and  $S_i = \sum_k^{K_i} S_k$  is the interfacial part of  $\mathfrak{R}_i$  assembled of  $K_i$  interfaces  $S_k$  associated phase  $i$ . Now the generalized transport theorem [1] is applied to determine each derivative of as

$$\frac{d\Phi_{V_i}(t)}{dt} = \frac{d}{dt} \int_{V_i(t)} \eta_i(\underline{z}, t) dV = \int_{R_i} \frac{\partial \eta_i}{\partial t} dV + \int_{R_i} \eta_i \mathbf{V}_{R_i} \cdot \mathbf{n}_i dA + \sum_k^{K_i} \int_{S_k} \eta_{i \rightarrow S_k} \mathbf{U}_k \cdot \mathbf{n}_k dA \quad (10)$$

where boundaries  $R_i$  and  $S_k$  (Fig. 3) are moving at velocities  $\mathbf{V}_{R_i}$  and  $\mathbf{U}_k$ , respectively.  $\mathbf{n}_i$  and  $\mathbf{n}_k$  are the unit normal vectors to boundaries  $R_i$  and  $S_k$ , ( $k = 1, 2$ ), respectively, drawn outward with respect to  $V_i(t)$ .  $\eta_{i \rightarrow S_k}$  is the spatial density of EQ stored in the  $i^{th}$  phase taken at infinitesimally close position to interface  $S_k$ . Eq. (10) can be modified by the use of the Gauss's theorem [3]. Thus one obtains

$$\int_{R_i} \eta_i \mathbf{V}_{R_i} \cdot \mathbf{n}_i dA + \sum_k^{K_i} \int_{S_k} \eta_{i \rightarrow S_k} \mathbf{U}_k \cdot \mathbf{n}_k dA = \int_{V_i} \text{div}(\eta_i \mathbf{V}_{\mathfrak{R}_i}) dV \quad (11)$$

By substitution Eq. (11) into Eq. (10) and subsequently Eq. (10) into Eq. (9) one gets

$$\frac{d\Phi_V(t)}{dt} = \sum_i^3 \int_{V_i} \frac{\partial \eta_i}{\partial t} dV + \sum_i^3 \int_{V_i} \text{div}(\eta_i \mathbf{V}_{\mathfrak{R}_i}) dV = \int_V \frac{\partial \eta}{\partial t} dV + \int_V \text{div}(\eta \mathbf{V}_{\mathfrak{R}}) dV \quad (12)$$

**Term (2)**

The rate of accumulation in system by moving spatial subsystems relative to the CV refers to phases engaged in spatial regions  $I$  and  $II$ . Hence Term (2) of Eq. (6) is

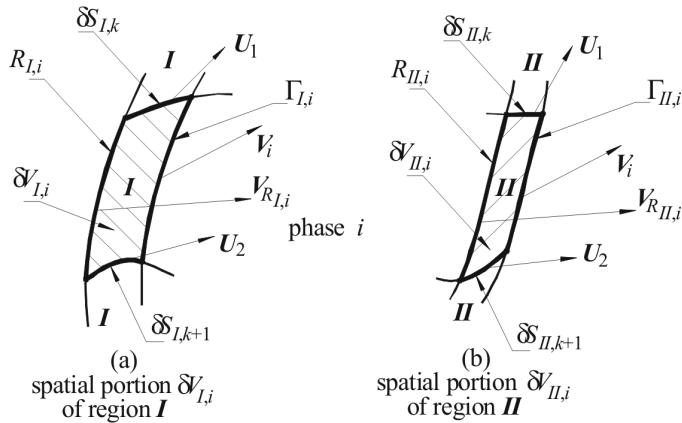


Fig. 4. The spatial portions of region I of volume  $\delta V_{I,i}$  and region II of volume  $\delta V_{II,i}$ , accompanied by associated boundaries

$$\lim_{\delta t \rightarrow 0} \frac{\delta_V \Phi_{II}(\delta t) - \delta_V \Phi_I(\delta t)}{\delta t} = \lim_{\delta t \rightarrow 0} \frac{\sum_i \delta t \frac{d\Phi_{II,i}}{dt} - \sum_i \delta t \frac{d\Phi_{I,i}}{dt}}{\delta t} \quad (13)$$

Below each derivative  $d\Phi_{I,i}/dt$  of Eq. (13) referenced to the  $i^{th}$  spatial portion of region I of volume  $\delta V_{I,i}$  bounded by  $\Gamma_{I,i} \cup R_{I,i} \cup \delta S_{I,i}$ , (Fig. 4a), is determined by the generalized transport theorem [1]. Hence one gets

$$\frac{d\Phi_{I,i}}{dt} = \int_{\delta V_{I,i}} \frac{\partial \eta_i}{\partial t} dV - \int_{\Gamma_{I,i}} \eta_i V_i \cdot \mathbf{n}_i dA + \int_{R_{I,i}} \eta_i V_{R_i} \cdot \mathbf{n}_i dA + \sum_k \int_{\delta S_{I,k}} \eta_i V_k \cdot \mathbf{n}_k dA \quad (14)$$

where  $\delta S_{I,k}$  is the  $k^{th}$  portion of  $\delta S_{I,i}$  and  $\delta S_{I,i} = \sum_k \delta S_{I,k}$  (Fig. 4a).

Likewise, for the  $i^{th}$  spatial portion of region II of volume  $\delta V_{II,i}$  bounded by  $\Gamma_{II,i} \cup R_{II,i} \cup \delta S_{II,i}$ , (Fig. 4b), one gets accumulation rate  $d\Phi_{II,i}/dt$  given as

$$\frac{d\Phi_{II,i}}{dt} = \int_{\delta V_{II,i}} \frac{\partial \eta_i}{\partial t} dV + \int_{\Gamma_{II,i}} \eta_i V_i \cdot \mathbf{n}_i dA - \int_{R_{II,i}} \eta_i V_{R_{II,i}} \cdot \mathbf{n}_i dA + \sum_k \int_{\delta S_{II,k}} \eta_i V_k \cdot \mathbf{n}_k dA \quad (15)$$

where  $\delta S_{II,k}$  is the  $k^{th}$  portion of  $\delta S_{II,i}$  and  $\delta S_{II,i} = \sum_k \delta S_{II,k}$  (Fig. 4b). By substitution Eqs (14, 15) into Eq. (13) and letting  $\delta t \rightarrow 0$  one obtains Term (2) of Eq. (6) in the rate form given as

$$\lim_{\delta t \rightarrow 0} \frac{\delta_V \Phi_{II}(\delta t) - \delta_V \Phi_I(\delta t)}{\delta t} = \sum_i \int_{P_i} \eta_i (V_i - V_{R_i}) \cdot \mathbf{n}_i dA = \int_R \eta (V - V_{R_i}) \cdot \mathbf{n} dA \quad (16)$$

where  $R_i = R_{I,i} + R_{II,i}$  is the external boundary of the phasic volume  $V_i$ .

**Term (3)**

By letting  $\delta t \rightarrow 0$  and taking the limit the rate form of Term (3) of Eq. (8) is

$$\lim_{\delta t \rightarrow 0} \frac{\Phi_S(t + \delta t) - \Phi_S(t)}{\delta t} = \frac{d\Phi_S(t)}{dt} = \sum_k \frac{d\Phi_{S_k}}{dt} \quad (17)$$

Storage  $\Phi_{S_k}(t)$  in the interface of area  $S_k(t)$  at an instant  $t$  is described by an integral

$$\Phi_{S_k}(t) = \int_{S_k(t)} \eta_s(y^1, y^2, t) \sqrt{a(y^1, y^2, t)} dy^1 dy^2 \quad (18)$$

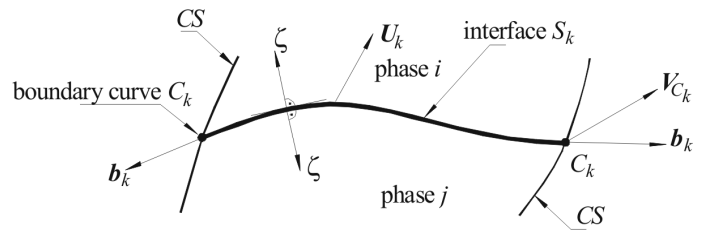


Fig. 5. Interface  $S_k$  between two phases – see description in the text

where  $a$  is the determinant of the surface metric tensor and  $y^1, y^2$  are the surface coordinates. Hence, rate  $d\Phi_{S_k}/dt$  of Eq. (17) is given now by the surface transport theorem [4]

$$\frac{d\Phi_{S_k}}{dt} = \int_{S_k} \left( \frac{\partial \eta_{s,k}}{\partial t} + \eta_{s,k} \text{div}_s U_k \right) dA + \oint_{C_k} \eta_{s,k} (V_{C_k} - U_k) \cdot \mathbf{b}_k dl \quad (19)$$

where  $dA = \sqrt{a} dy^1 dy^2$  and  $\text{div}_s U_k$  is the surface divergence of  $U_k$ ,  $V_{C_k}$  is the spatial velocity of  $C_k$ ,  $\mathbf{b}_k$  is the unit surface vector (tangent to  $S_k$ ) normal to  $C_k$  directed outward of  $S_k$  (Fig. 5).

By substitution Eq. (19) into Eq. (17), taking the limit and performing summation one gets Term (3) of Eq. (6) given by

$$\lim_{\delta t \rightarrow 0} \frac{\Phi_S(t + \delta t) - \Phi_S(t)}{\delta t} = \int_S \left( \frac{\partial \eta_s}{\partial t} + \eta_s \text{div}_s U \right) dA + \oint_C \eta_s (V_C - U) \cdot \mathbf{b} dl \quad (20)$$

**Term (4)**

By letting  $\delta t \rightarrow 0$  and taking the limit the rate form of the 4<sup>th</sup> term of Eq. (6) is

$$\lim_{\delta t \rightarrow 0} \frac{\delta_S \Phi_{II}(\delta t) - \delta_S \Phi_I(\delta t)}{\delta t} = \lim_{\delta t \rightarrow 0} \frac{\sum_{\kappa} \delta t \frac{\Phi_{II,\kappa}^{(s)}}{dt} - \sum_{\kappa} \delta t \frac{\Phi_{I,\kappa}^{(s)}}{dt}}{\delta t} \quad (21)$$

Consequently accumulation rate  $d\Phi_{I,k}^{(s)}/dt$  in the interface portion  $\delta S_{I,k}$ , (Fig. 6a), is (generalized surface transport theorem [2])

$$\frac{d\Phi_{I,k}^{(s)}}{dt} = \int_{\delta S_{I,k}} \left( \frac{\partial \eta_{s,k}}{\partial t} - \text{grad}_s \eta_{s,k} \cdot U_k - 2H_k \eta_{s,k} U_k \cdot \zeta_k \right) dA + \oint_{C_{I,k}} \eta_{s,k} V_{C_k} \cdot \mathbf{b}_k dl - \oint_{I_{I,k}} \eta_{s,k} V_{s,k} \cdot \mathbf{b}_k dl \quad (22)$$

where  $V_{s,k}$  is the spatial velocity of the surface system flowing in  $\delta S_{I,k}$  and  $H_k$  is the mean curvature of  $\delta S_{I,k}$ ,  $I_{I,k}$  is the bound-

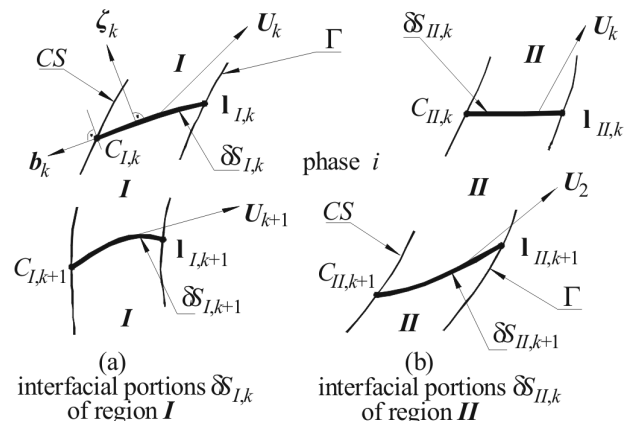


Fig. 6. Interfacial portions  $\delta S_{I,k}$  and  $\delta S_{II,k}$ , ( $k = 1, 2$ ), of region I and region II, respectively, accompanied by associated boundaries

dary curve formed by intersection of system boundary  $\Gamma$  and  $S_k$ .

Likewise, accumulation rate  $d\Phi_{II,k}^{(S)}/dt$  in interface portion  $\delta S_{II,k}$  located in region **II**, (Fig. 6b), is

$$\frac{d\Phi_{II,k}^{(S)}}{dt} = \int_{\delta S_{II,k}} \left( \frac{\partial \eta_{s,k}}{\partial t} - \text{grad}_s \eta_{s,k} \bullet \mathbf{U}_k - 2H_k \eta_{s,k} \mathbf{U}_k \bullet \boldsymbol{\zeta}_k \right) dA - \int_{C_{II,k}} \eta_{s,k} \mathbf{V}_{C_k} \bullet \mathbf{b}_k dl + \int_{II,k} \eta_{s,k} \mathbf{V}_{s,k} \bullet \mathbf{b}_k dl \quad (23)$$

By substitution Eqs (22, 23) into Eq. (21) and letting  $\delta t \rightarrow 0$  one finds Term (4) of Eq. (6) becomes to be expressed in the rate form as

$$\lim_{\delta t \rightarrow 0} \frac{\delta_s \Phi_{II}(\delta t) - \delta_s \Phi_I(\delta t)}{\delta t} = \sum_k^K \int_{C_{II,k}} \eta_{s,k} (\mathbf{V}_{s,k} - \mathbf{V}_{C_k}) \bullet \mathbf{b}_k dl = \int_C \eta_s (\mathbf{V}_s - \mathbf{V}_C) \bullet \mathbf{b} dl \quad (24)$$

By substitution expression (7) onto left side of Eq. (6) and relations (12), (16), (20) and (24) into the right side of Eq. (6) we can generalize the *RTT* for three phase systems as follows

$$\frac{d\Phi_{\Sigma}}{dt} = \underbrace{\int_V \frac{\partial \eta}{\partial t} dV + \int_V \text{div}(\eta \mathbf{V}_{\mathfrak{R}}) dV + \int_R \eta (\mathbf{V} - \mathbf{V}_R) \bullet \mathbf{n} dA}_{\text{phasic terms}} + \underbrace{\int_S \left( \frac{\partial \eta_s}{\partial t} + \eta_s \text{div}_s \mathbf{U} \right) dA + \int_C \eta_s (\mathbf{V}_C - \mathbf{U}) \bullet \mathbf{b} dl + \int_C \eta_s (\mathbf{V}_s - \mathbf{V}_C) \bullet \mathbf{b} dl}_{\text{interfacial terms}} \quad (25)$$

The third term on the right side of Eq. (25) can be modified by the use of the *Gauss's* theorem for spatial domains [3]. Thus one gets

$$\int_R \eta (\mathbf{V} - \mathbf{V}_R) \bullet \mathbf{n} dA = \int_V \text{div}[\eta (\mathbf{V} - \mathbf{V}_{\mathfrak{R}})] dV + \int_S \|\eta_{\triangleright S} (\mathbf{V}_{\triangleright S} - \mathbf{U}) \bullet \boldsymbol{\zeta}\| dA \quad (26)$$

where

$$\int_S \|\eta_{\triangleright S} (\mathbf{V}_{\triangleright S} - \mathbf{U}) \bullet \boldsymbol{\zeta}\| dA = \sum_k^K \int_{S_k} \|\eta_{\triangleright S_k}^+ (\mathbf{V}_{\triangleright S_k}^+ - \mathbf{U}_k) \bullet \boldsymbol{\zeta}^+ + \eta_{\triangleright S_k}^- (\mathbf{V}_{\triangleright S_k}^- - \mathbf{U}_k) \bullet \boldsymbol{\zeta}^-\| dA \quad (27)$$

Substitution of Eq. (26) into Eq. (25) yields the final form of the *RTT* attempted as follows

$$\begin{aligned} \frac{d\Phi_{\Sigma}}{dt} = & \underbrace{\int_V \frac{\partial \eta}{\partial t} dV + \int_V \text{div}(\eta \mathbf{V}_{\mathfrak{R}}) dV}_{\text{accumulation in } \Sigma} + \underbrace{\int_V \text{div}[\eta (\mathbf{V} - \mathbf{V}_{\mathfrak{R}})] dV}_{\text{accumulation in moving spatial phasic domains of volume } V} + \underbrace{\int_S \left( \frac{\partial \eta_s}{\partial t} + \eta_s \text{div}_s \mathbf{U} \right) dA + \int_C \eta_s (\mathbf{V}_C - \mathbf{U}) \bullet \mathbf{b} dl}_{\text{accumulation of interfacial domains of area } S} + \\ & \underbrace{\int_C \eta_s (\mathbf{V}_s - \mathbf{V}_C) \bullet \mathbf{b} dl}_{\text{transport of EQ by movement of surface subsystems across bounding curves } C} + \underbrace{\int_S \|\eta_{\triangleright S} (\mathbf{V}_{\triangleright S} - \mathbf{U}) \bullet \boldsymbol{\zeta}\| dA}_{\text{transport between interface } S \text{ and bulk phases}} \quad (28) \end{aligned}$$

In this notation subscript  $\triangleright S_k$  stands for value of a phasic property referenced at infinitesimally close spatial position to  $S_k$ . Note also in Eq. (28) the spatial divergence operator  $\text{div}$  and surface divergence operator  $\text{div}_s$  are different, see formulas for these operators given by *Slattery* [2].

### Concluding remarks

The *RTT* is a basic tool in development of the local instantaneous model equations together with corresponding jump conditions based on which averaged models can be derived. The form of *RTT* given by Eq. (28) is the most general because it expresses the rate of accumulation in a three phase system in terms of moving and deformable *CV* of arbitrary prescribed configuration in which *EQ* can be accumulated both by the phases and interface. Worthy to mention is applicability of *RTT* relation developed also to multiphase systems provided that particular terms can account in contributions done by all spatial and surface subsystems involved.

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